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Relation between Transfer of CO₂ and the pH of the Medium

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Authors' contributions

This work was carried out in collaboration between all authors. Author JAVC designed the study and managed the literature searches. Author FVC managed the analyses, performed the statistical analysis and wrote the manuscript. All authors read and approved the final manuscript.

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ABSTRACT

Microalgae are great users of $CO₂$ and can fix large amounts of this compound. In algal biomass production systems, the requirement of carbon is usually supplied by $CO₂$, continuously or intermittently. The relative concentrations of inorganic carbon species determine the pH and, in turn, are determined by the pH of the medium. This study aimed to establish a relation between the variation in $CO₂$ concentration and the pH of the medium and validate the equation proposed for the transfer of $CO₂$ during the supply of this gas in the liquid medium in a carbon dioxide biofixation process in an open raceway type bioreactor, provided with a carbon dioxide injection system. The experiments were performed in a 200 L open raceway type bioreactor, in which a gas injection system was used where air enriched with 12% CO_{2} (VV) at a specific flow rate of 0.05 min⁻¹. An equation was established to determine the pH variation from the variation of the $CO₂$ concentration in the environment. The data obtained from the proposed equation were satisfactorily explained by experimental data (r^2 = 0.90).

Keywords: CO2; supply; pH; microalgae.

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1. INTRODUCTION

The photoautotrophic growth of microalgae requires the supply of $CO₂$ as a carbon source. At the same time, the supply of $CO₂$ helps to control the pH of the culture. Chemical analyses show that microalgal biomass contains 40 to 50% of carbon, which suggests that approximately 1.5 to 2.0 kg of carbon dioxide is needed to produce 1.0 kg of biomass [9].

The transfer of $CO₂$ into the culture medium is a factor that has been gaining attention in studies in chemical and biochemical engineering. Theoretical and experimental correlations have been well developed. However, they only provide approximate and/or relative estimates of transfer rates. In the final analysis, these rates must be empirically determined from prototypes and pilots. This is especially true for the carbonation of open ponds, where instances of irregular surfaces are frequent due to turbulence, wind and bubbles. These disturbances may cause a significant effect on gas transfer in tanks [1].

The generally used explanation for the mechanism of gas transfer is the dual-film theory. According to this theory, there are two films, a liquid and a gas, the gas-liquid interface promotes most of the resistance against the passage of gas molecules from the gas phase to the liquid phase. For high solubility gases in the liquid phase, for example, absorption of $SO₂$ in water, the main absorption resistance is offered by the gas film. For low solubility gases in the liquid phase, for example, absorption of oxygen and $CO₂$ in aqueous solutions, the resistance is limited by the liquid film. For intermediate solubility gases, both films can offer significant resistance [6].

The predominant chemical reactions in the culture medium used to obtain microalgal biomass are presented below:

$$
CO_2 + OH^- \leftarrow^{k} + HCO_3^-
$$

\n
$$
CO_2 + H_2O \leftarrow^{k} + HCO_3^- + H^+
$$

\n
$$
HCO_3^- + OH^- \leftarrow^{k} \rightarrow CO_3^{2-} + H_2O
$$

\n
$$
HCO_3^- \leftarrow^{k} \rightarrow CO_3^{2-} + H^+
$$

\n
$$
H_2O \leftarrow^{k} \rightarrow H^+ + OH^-
$$

The relationship between the chemical species of inorganic carbon and pH of the medium may be expressed by the dissociation constants K_1 and K₂, shown in Equations 1 and 2.

$$
K_1 = \frac{H^+ \cdot HCO_3^-}{H_2CO_3^*}
$$
 Equation 1

$$
K_2 = \frac{H^+ \cdot CO_3^{-2}}{HCO_3^-}
$$
 Equation 2

Where, according to Carmouze (1994) [2]:

$$
K_1 = 4,4361x10^{-7}
$$

\n
$$
K_2 = 4,6881x10^{-11}
$$

\n
$$
\alpha_0 = \frac{1}{\left(1 + \left(\frac{K_1}{H^+}\right) + \frac{K_1K_2}{H^{+2}}\right)}
$$
 Equation 3

Equation 4

$$
A = \frac{1}{\left(1 + \left(\frac{H^+}{K_1}\right) + \frac{K_2}{H^+}\right)}
$$

$$
B = \frac{1}{\left(\frac{H^+}{K_1} + \frac{1}{K_2} + \frac{1}{K_1}\right)}
$$

 $\alpha_1 = \frac{1}{\sqrt{1-\frac{1}{2}}}$

I L \setminus L L \setminus K_1K *H*

ſ $^{+}$

 2^{-} $(1 + x + 2)$ 1

ſ

α

Equation 5

$$
CO_2 = \alpha_0 * CT
$$
 Equation 6

K H

 $\vert +$ $\overline{}$ J

 $1^{\mathbf{A}}2$ \mathbf{A}^2

 \mathcal{L}

 $\overline{}$ I J

 \backslash

$$
HCO_3^- = \alpha_1 * CT
$$
 Equation 7

$$
CO_3^{-2} = \alpha_2 \cdot CT
$$
 Equation 8

Where CT is the total concentration of inorganic carbon in the medium.

Production of OH- occurs in the conversion of both bicarbonate and carbonate to $CO₂$, increasing the medium pH. For this reason, in an intensive cultivation of microalgae, it is not possible to achieve complete consumption of the substrate present in the medium without pH correction, since it reaches values close to 14, inhibiting the growth of microalgae [7].

This study aimed to establish a relation between the change in $CO₂$ concentration and the pH of the medium and validate the proposed equation for the transfer of $CO₂$ during the supply of this gas in the liquid medium in a process of carbon dioxide biofixation in an open raceway bioreactor, provided with a carbon dioxide injection system.

2. MATERIALS AND METHODS

2.1 CO₂ Supply System

The determinations of the $CO₂$ global transfer coefficient (k_La_{CO2}) were performed in an open raceway bioreactor (2.50 \times 0.70 \times 0.40 m) with 200 L volume capacity, in which a gas injection system was used (Fig. 1) where enriched air with 12% $CO_{2 (V/V)}$ was injected into the medium at a specific flow rate 0.05 min⁻¹. This system was used to provide a homogeneous distribution of the mass transferred to the liquid medium (fresh water in this case). coefficient (k_L a_{co2}) were performed in an open
raceway bioreactor (2.50 x 0.70 x 0.40 m) with
200 L volume capacity, in which a gas injection
system was used (Fig. 1) where enriched air with
12% CO_{2 (V/V)} was inject

The determination of the volumetric coefficient of oxygen transfer (k_La_{O2}) was performed according to the methodology proposed by Schmidell (2001) [8]. The method is based on the reduction of dissolved oxygen concentration by addition of sodium sulfite $(Na₂SO₃)$. Subsequently, air injection is performed under the conditions to measure dissolved oxygen concentration.

ETHODS

The determination of the coefficient of volumetric

transfer of carbon dioxide (k₁a_{coz}) was

performed according to the methodology

proposed by Talbot (1990) [10]. The author

performed in an open k₁a_{co} transfer of carbon dioxide (k_La_{CO2}) was performed according to the methodology proposed by Talbot (1990) [10]. The author determined the relationship between $k_{L}a_{CO2}$ and k_La_{O2} by Equation 9 [11]. methodology
The author
n k_La_{CO2} and

$$
k_L a_{CQ_2} = k_L a_{Q_2} * \sqrt{\frac{D_{Q_2}}{D_{CQ_2}}}
$$
 Equation 9

2.2 Analytical Determinations Determinations

The pH was determined with a digital pH meter (QUIMIS Q400H, Brazil). The pH was determined with a digital pH meter
(QUIMIS Q400H, Brazil).
Measurements of clissolved oxygen
concentration were guided using a dissolved

Measurements of dissolved oxygen oxygen meter (Orion Model 510A, USA) at 25°C.

Fig. 1. CO2 Supply System

3. RESULTS AND DISCUSSION

Isolating H^+ in Equation 10:

$$
K_1 = \frac{H^+ \cdot HCO_3^-}{H_2CO_3^*}
$$
 Equation 10

Where:

$$
HCO_3^- = \alpha_1 \cdot CT
$$
 Equation 11

In which:

$$
\alpha_1 = \frac{1}{\left(1 + \left(\frac{H^+}{K_1}\right) + \frac{K_2}{H^+}\right)}
$$
 Equation 12

Correlating the pH variation with the variation in $CO₂$ concentration, considering that the $concentration$ of $HCO₃⁻$ does not vary significantly at each time interval and that $H_2CO_3^*$ represents the sum of the concentration of $CO₂$ and $H₂CO₃$, with the concentration of $CO₂$ being approximately 250 times greater than H_2CO_3 [2], so $H_2CO_3^*$ was regarded as the CO_2 concentration in the liquid medium. Thus, replacing the right side of Equations 11 and 12 in Equation 10:

$$
H_t^+ = H_0^+ + \frac{K_1 * (CO_2 - CO_2^0)}{\left(\frac{1}{\left(1 + \frac{H_0^+}{K_1}\right) + \frac{K_2}{H_0^+}}\right) * CT_t}
$$
 Equation 13

Considering that during the injection of $CO₂$ in the liquid medium, the mass balance for this component may be given by Equation 14, values of $CO₂$ as a function of time (Fig. 2) were plotted.

$$
\frac{dCO_2}{dt} = kla \cdot (CO_2^{Sat} - CO_2)
$$
 Equation 14

Where:

 k_1 a= 96 d⁻¹ (determined experimentally)

 CO_2 ^{Sat} - CO_2 concentration at saturation with the gas phase that represents parts of $CO₂$ in parts of H_2O [4].

$$
CO_2^{Sat} = \left(\frac{x_{CO_2}}{1 - x_{CO_2}}\right) * \left(\frac{M_{CO_2}}{M_W}\right)
$$
 Equation 15

Where:

 x_{CO2} - Molar fraction of $CO₂$ in the saturated medium

$$
x_{CO2} = \frac{p_{CO_2}}{H_{CO_2}}
$$
 Equation 16

- p_{CO_2} Partial pressure of CO₂ in the saturated medium (atm)
- H_{CO_2} Henry constant for CO₂at medium temperature (atm⁻¹)
- ${M}_{CO_2}$ Molar mass of CO₂ (44)
- ${M}_{\it W}~$ Molar mass of water (18)

In order to validate the proposed equation, pH values versus time obtained from Equation 13 and the values obtained experimentally during the injection of $CO₂$ into the medium were plotted. Fig. 3 shows the values simulated from Equation 13 and observed experimentally for pH versus time.

Grima et al. [3] established an equation for the transfer of $CO₂$ in tubular photobioreactors. These authors confirmed the application of the theory of the liquid film when $CO₂$ is injected into seawater through an air-lift $CO₂$ supply system.

Talbot et al. [10] concluded that the physicochemical conditions presented in algal biomass culture medium (presence of OH, H_2O and NH₃) did not significantly affect the coefficient of mass transfer of $CO₂$, their reactions can be neglected. Thus, they determined that the volumetric coefficient of mass transfer of $CO₂$ (k_La_{CO2}) can be calculated from the $k_{L}a_{O2}$ by a correction factor involving the diffusivity of both gases in water.

Putt et al. [5] developed an absorption column in order to absorb 90% of supplied $CO₂$. These authors concluded that the best results obtained (82%) occurred in media containing low alkalinity (pH 8-9).

Fig. 2. CO₂ concentration in the medium as a function of time

Fig. 3. pH values versus time during the supply of CO₂ in the medium

Fig. 4 shows the values predicted by Equation 13 as a function of the experimentally observed values.

Fig. 5 shows simulated values of pH versus time at different initial conditions for the total dissolved inorganic carbon, pH and $CO₂$.

To make the microalgal growth viable at satisfactory rates, it is necessary to maintain the pH within the ideal range, specific for each microorganism. According to Benemann et al. [1], buffering the system with respect to $CO₂$ injection system depends on the range of variation of pH. The buffering capacity is at a minimum at about pH 8.3 where the bicarbonate is the dominant species. In both, it increases above and below this region, though at a higher rate in the acidic region. Thus, algae having the ability to grow in media with pH between 6 and 7.5 require less alkalinity for the same carbon storage. Furthermore, the fraction of the total inorganic carbon in the form of carbonate decreases approximately at a factor of 10 for every decrease in one pH unit (between pH 7 to 10). On the other hand, the fraction of $CO₂$ decreases 10 times with each increase in pH in this range, tending to minimize problems with loss of $CO₂$ to the atmosphere at high pH.

Fig. 4. Values predicted by equation 13 according to the experimentally observed pH values

Fig. 5. pH versus time (values simulated from equation 13)

4. CONCLUSIONS

The results show that it is possible to determine the behavior of pH from $CO₂$ values. In processes of $CO₂$ biofixation, the relation between the variation of $CO₂$ and variation in the pH of the medium makes it possible to establish control of these factors.

The determination of the volumetric mass transfer coefficient for the gas injection system used in a $CO₂$ biofixation processes can be performed based on the values obtained for oxygen.

COMPETING INTERESTS

Authors have declared that no competing interests exist.

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